

MECE 3350U
Control Systems

Lecture 9
Dominant Poles and Zeros

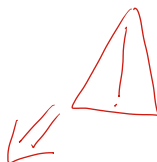
Midterm exam - Section 15

When: Monday, Oct 15, 11:10-12:30

What: Lectures 1 to 8

Where: Room split by **first** name:

A-I	J-Z
UL9	UA2120



Prepare your formula sheet (1 page, letter size, both sides)

Everything must be handwritten

Your formula sheet cannot exceed 1 page (letter size), both sides.

Please write your name/student ID on the formula sheet

→ Bring a photo ID or student card.

→ Exam problems are in line with those solved in class, tutorials, and assignments.

→ Office hours during the reading week: As usual.

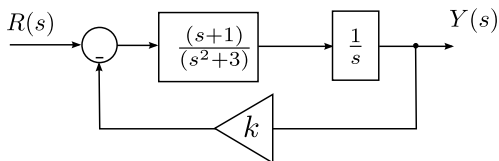
Outline of Lecture 9

By the end of today's lecture you should be able to

- Understand the concept of dominant poles
- Recognize the influence zeros on the transient response
- Simplify a transfer function to lower orders

Applications

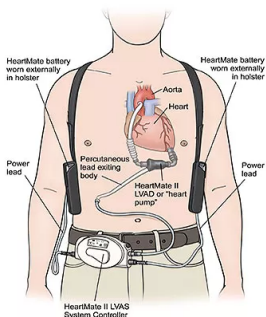
The roll control autopilot of an aircraft has the following structure:



How can we calculate the k that yields an overshoot of less than 2%?

Applications

A ventricular assist device is a mechanical pump used to support heart function and blood flow in people with weak or failing hearts.



The model of the heart and pump system results in a third order transfer function. How can we analyse the transient response of the system?

First order system

Consider the response of a first order system to an unit step input:

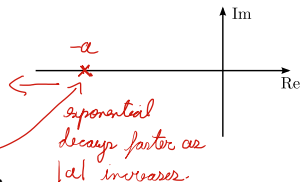
$$X(s) = \frac{1}{s+a} \left(\frac{1}{s} \right)$$

Using partial fraction expansion:

$$X(s) = \frac{1/a}{s} - \frac{1/a}{s+a}$$

The inverse transform yields

$$x(t) = \frac{1}{a}(1 - e^{-at})$$



The transfer function has one pole located at $s = -a$.

→ How does the magnitude of $s = -a$ influence the transient response?

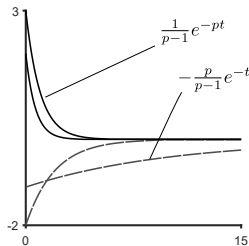
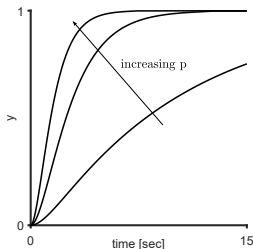
The effect of an additional pole

Let us now examine the step response of

$$X(s) = \frac{p}{(s+1)(s+p)} \left(\frac{1}{s} \right) = \frac{1}{(s+1)\left(\frac{1}{p}s+1\right)} \left(\frac{1}{s} \right).$$

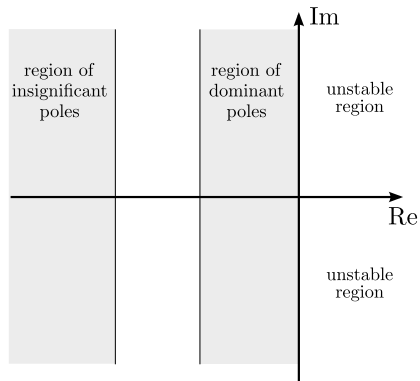
Partial fraction expansion gives:

$$y(t) = 1 - \frac{p}{p-1}e^{-t} + \frac{1}{p-1}e^{-pt}$$



Conclusion: If $p \gg 1$, the term $1/(p-1)e^{-pt}$ is negligibly small as $t \rightarrow \infty$.

The effect of an additional pole



If the magnitude of the real part of a pole is at least 5 to 10 times that of a dominant pole, then the pole may be regarded as insignificant.

Second order systems with an additional pole

Consider the 3rd order function

$$T(s) = \frac{1}{(s^2 + 2\zeta\omega_n s + 1)(\gamma s + 1)}.$$

Real part of the poles are: $-1/\gamma$ and $-\zeta\omega_n$. Thus, if

$$\left| \frac{1}{\gamma} \right| \geq 10|\zeta\omega_n| \quad (1)$$

The response can be approximated by

$$T_a(s) = \frac{1}{s^2 + 2\zeta\omega_n s + 1}.$$

Take $\omega_n = 1$, and $\zeta = 0.45$: gives two poles at $s = -0.45 \pm 0.89i$.

Example 1: $\gamma = 1.00 \rightarrow$ Adds a pole to $s = -1$

Example 2: $\gamma = 0.22 \rightarrow$ Adds a pole to $s = -4.5$.

Example 3: $\gamma = 0.10 \rightarrow$ Adds a pole to $s = -10$.

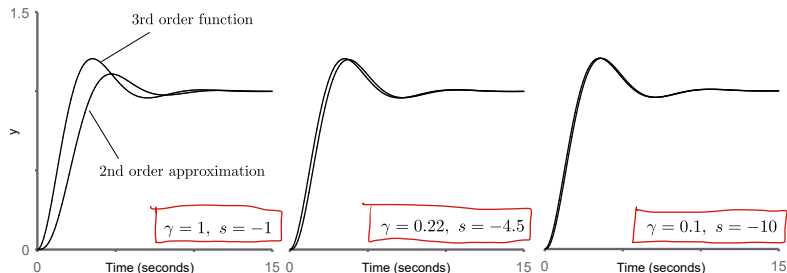
Second order systems with an additional pole

Original 3rd order function:

$$T(s) = \frac{1}{(s^2 + 2\zeta\omega_n s + 1)(\gamma s + 1)}$$

2nd order approximation:

$$T_a(s) = \frac{1}{s^2 + 2\zeta\omega_n s + 1}$$



Additional zeros

Consider the transfer function with an additional zero $s = -z$:

$$\frac{Y(s)}{R(s)} = \frac{\frac{\omega_n^2}{z}(s+z)}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (2)$$

If $z \gg \zeta\omega_n$, the zero will have minimal effect on the step response.

The unit step response of the above equation is:

$$\frac{Y(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} + \frac{\frac{\omega_n^2}{z}s}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (3)$$

If $x(t)$ is the inverse of the first term, then the time response is

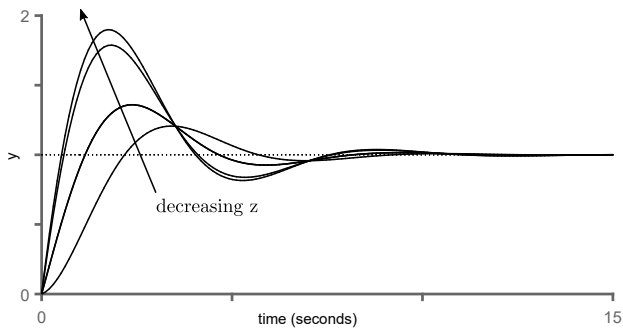
$$y(t) = x(t) + \frac{1}{z} \left(\frac{d}{dt} x(t) \right) \quad (4)$$

Conclusion: The additional zero speeds up transients, making rises and falls sharper.

Additional zeros

$$\frac{Y(s)}{R(s)} = \frac{\frac{\omega_n^2}{z}(s+z)}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (5)$$

Consider: $\omega_n = 1$, $\zeta = 0.45$, $z = 0.7, 1, 10$



Simplification to a lower order

A more precise approach: Match the frequency response.

*for information
only.*

Consider the high order system:

$$G_H(s) = K \frac{a_m s^m + a_{m-1} s^{m-1} + \dots + a_1 s + 1}{b_n s^n + b_{n-1} s^{n-1} + \dots + b_1 s + 1} \quad (6)$$

with $m \geq n$, which is to be mapped to a lower order system

$$G_L(s) = K \frac{c_p s^p + c_{p-1} s^{p-1} + \dots + c_1 s + 1}{d_g s^g + d_{g-1} s^{g-1} + \dots + d_1 s + 1} \quad (7)$$

such that $p \leq g \leq n$.

The c and d coefficients of the approximate solution G_L are obtained via

$$M^k = \frac{d^k}{ds^k} M(s) \quad (8)$$

$$\Delta^k = \frac{d^k}{ds^k} \Delta(s) \quad (9)$$

Simplification

*for information
only.*

Let us define

$$M_{2q} = \sum_{k=0}^{2q} \frac{(-1)^{k+q} M^k(0) M^{2q-k}(0)}{k!(2q-k)!} \quad (10)$$

$$\Delta_{2q} = \sum_{k=0}^{2q} \frac{(-1)^{k+q} \Delta^k(0) \Delta^{2q-k}(0)}{k!(2q-k)!} \quad (11)$$

So that the c and d coefficient are obtained by equating

$$M_{2q} = \Delta_{2q} \quad (12)$$

for $q = 1, 2, \dots$ and up to the number required to solve for the unknowns.

Location of poles

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

The poles are

$$s = \zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$$

$$s = -\sigma \pm j\omega_d$$

where $\sigma = \zeta\omega_n$, and $\omega_d = \omega_n\sqrt{1-\zeta^2}$

→ Poles are located at a radius ω_n

→ The angle to the imaginary axis is $\theta = \sin^{-1} \zeta$

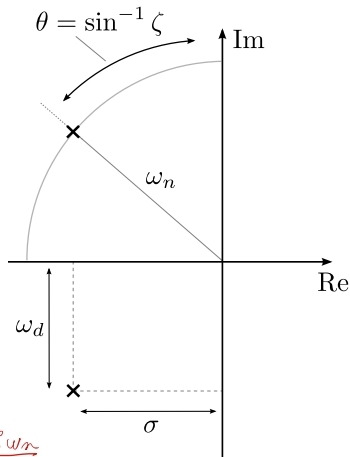
$$|s| = \sqrt{\sigma^2 + \omega_d^2}$$

$$|s| = \sqrt{\zeta^2\omega_n^2 + \omega_n^2(1-\zeta^2)}$$

$$|s| = \omega_n$$

$$\sin \theta = \frac{\sigma}{\omega_n} = \frac{\zeta\omega_n}{\omega_n}$$

$$\sin \theta = \zeta$$



Exercise 40

A closed-loop control system has a transfer function $T(s)$ as follows

$$T(s) = \frac{Y(s)}{R(s)} = \frac{2500}{(s + 50)(s^2 + 10s + 50)}.$$

Plot the time response to an unit step input when:

- **(a)** The actual $T(s)$ is used (use Matlab)
- **(b)** Using the dominant complex poles
- **(c)** Compare the results

Exercise 40 - continued

(a) The actual function is

$$T(s) = \frac{Y(s)}{R(s)} = \frac{2500}{(s+50)(s^2+10s+50)}$$

(b) The approximate transfer function is

$$T(s) = \frac{2500}{(s+50)(s^2+10s+50)}$$

$$T'(s) = \frac{50}{s^2+10s+50}$$

$$s' = -5 \pm 5j$$

$$50 \gg |-5|$$

can be neglected

⇒ Magnitude of $T'(s)$ and $T(s)$ must be the same.

Exercise 41

A closed-loop control system transfer function as two dominant complete conjugate poles. Sketch the region in the left-hand s-plane where the complex poles should be located to meet the given specifications:

$$\rightarrow \text{(a)} \quad 0.6 \leq \zeta \leq 0.8, \quad \omega_n \leq 10$$

$$\rightarrow \text{(b)} \quad 0.5 \leq \zeta \leq 0.707, \quad \omega_n \geq 10$$

$$\rightarrow \text{(c)} \quad \zeta \geq 0.5, \quad 5 \leq \omega_n \leq 10$$

$$\rightarrow \text{(d)} \quad \zeta \leq 0.707, \quad 5 \leq \omega_n \leq 10$$

$$\rightarrow \text{(e)} \quad \zeta \geq 0.6, \quad \omega_n \leq 6$$

Exercise 41 - continued

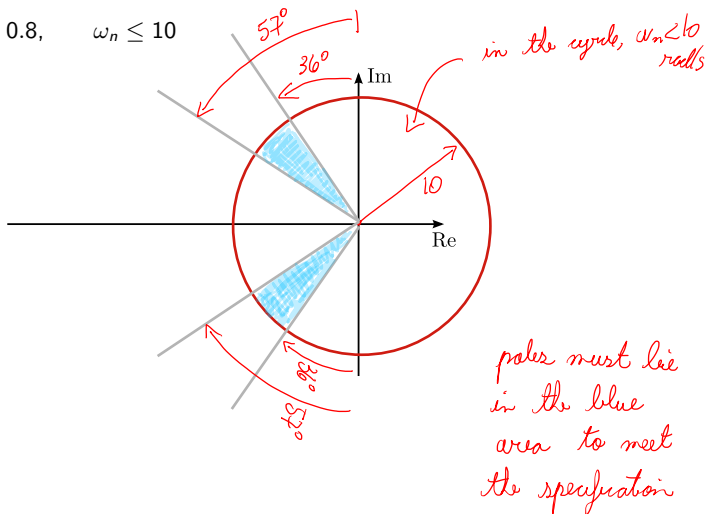
$$\rightarrow \text{(a)} \quad 0.6 \leq \zeta \leq 0.8, \quad \omega_n \leq 10$$

$$\theta_1 = \sin^{-1}(0.6)$$

$$\theta_1 = 36^\circ$$

$$\theta_2 = \sin^{-1}(0.8)$$

$$\theta_2 = 53^\circ$$



Exercise 41 - continued

→ (b) $0.5 \leq \zeta \leq 0.707$, $\omega_n \geq 10$

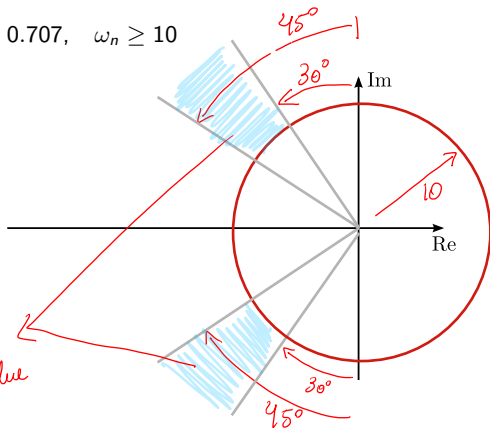
$$\theta_1 = \sin^{-1}(0.5)$$

$$\theta_1 = 30^\circ$$

$$\theta_2 = \sin^{-1}(0.707)$$

$$\theta_2 = 45^\circ$$

*poles are
in the blue
area.*



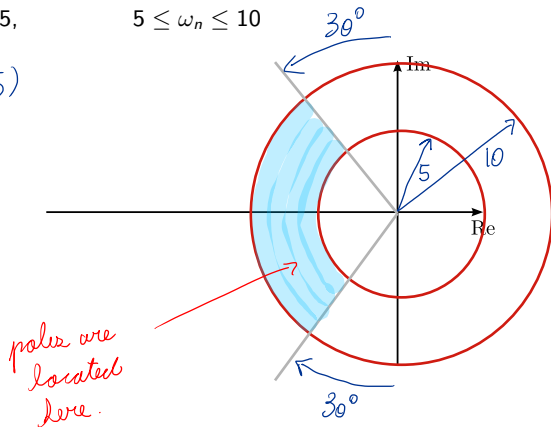
Exercise 41 - continued

$$\rightarrow \text{(c)} \zeta \geq 0.5,$$

$$5 \leq \omega_n \leq 10$$

$$\theta = \sin^{-1}(0.5)$$

$$\theta = 30^\circ$$

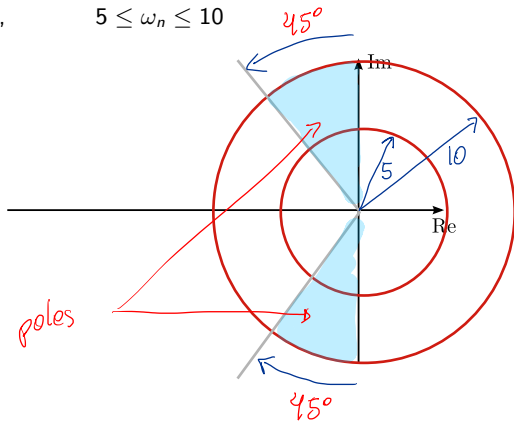


Exercise 41 - continued

$$\rightarrow \text{(d)} \quad \zeta \leq 0.707, \quad 5 \leq \omega_n \leq 10$$

$$\theta = \sin^{-1}(0.707)$$

$$\theta = 45^\circ$$

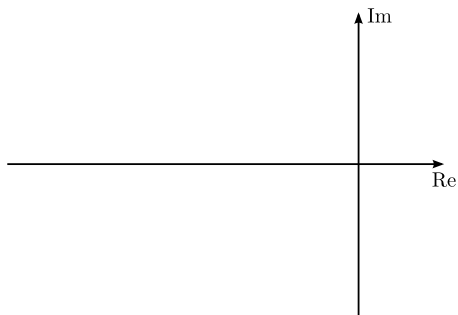


Exercise 41 - continued

$$\rightarrow \text{(e)} \zeta \geq 0.6,$$

$$\omega_n \leq 6$$

homework



Exercise 42

A closed-loop transfer function is

$$T(s) = \frac{Y(s)}{R(s)} = \frac{108(s+3)}{(s+9)(s^2+8s+36)}$$

- **(a)** Determine the steady state error for a unit step input.
- **(b)** Assume that the complex poles dominate and determine the percent overshoot and settling time.
- **(c)** Plot the actual system response and compare it with **(b)**

↳ Matlab code posted on BB

Exercise 42 - continued

(a) Steady-state error for $r(t) = 1$.

$$T(s) = \frac{Y(s)}{R(s)} = \frac{108(s+3)}{(s+9)(s^2+8s+36)} \cdot \frac{1}{s}$$

$$e_{ss} = 1 - \lim_{s \rightarrow 0} s \left(\frac{108(s+3)}{(s+9)(s^2+8s+36)} \cdot \frac{1}{s} \right)$$

$$e_{ss} = 1 - \frac{108 \times 3}{9 \times 36}$$

$$e_{ss} = 0 \quad (\checkmark \checkmark)$$

Exercise 42 - continued

(b) Overshoot and settling time considering the dominant poles.

$$T(s) = \frac{Y(s)}{R(s)} = \frac{108(s+3)}{(s+9)(s^2+8s+36)}$$

$$T'(s) = \frac{12(s+3)}{s^2+8s+36}$$

0 ←

$$\omega_n = \sqrt{36} = 6 \text{ rad/s}$$

$$2\zeta\omega_n = 8$$

$$\hookrightarrow \zeta = 0.67$$

$$\text{P.O.} = 100 e^{\frac{-\pi\zeta}{\sqrt{1-\zeta^2}}}$$

$$\boxed{\text{P.O.} = 6\%}$$

Exercise 42 - continued

(c) Overshoot and settling time considering the dominant poles.

$$T(s) = \frac{Y(s)}{R(s)} = \frac{108(s+3)}{(s+9)(s^2+8s+36)}$$

$$T_s = \frac{4}{\zeta \omega_n} = \frac{4}{0.6 \times 0.67}$$

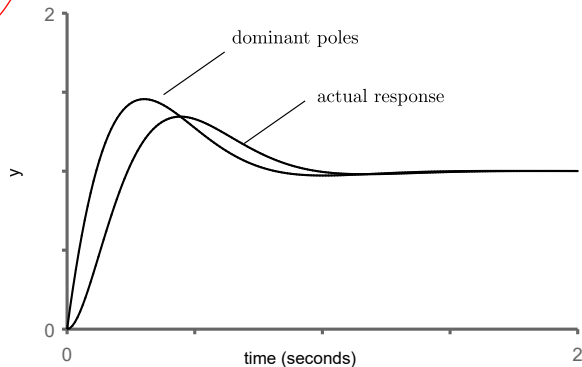
$$T_s = 1 \text{ sec}$$

Exercise 42 - continued

```
T = tf([108 324],[1 17 108 324]);  
step(T); stepinfo(T)
```

```
H = tf([108/9 324/9],[1 8 36]);  
step(H); stepinfo(H)
```

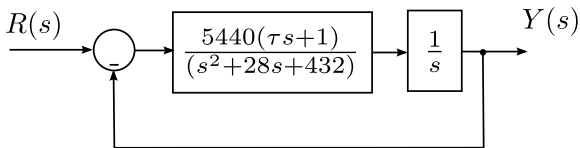
*Matlab posted on
Blackboard.*



Exercise 43

Homework.

Consider the following closed loop system

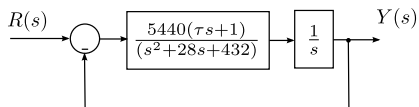


Where τ can take the values $\tau = 0, 0.05, 0.1$ or 0.5 . For $r(t) = 1$:

- **(a)** Record the percent overshoot, rise time, and settling time as τ varies.
- **(b)** Describe the effects of varying τ .
- **(c)** Compare the location of the zero with that of the closed-loop poles.

Exercise 43 - continued

The closed loop transfer function



*See next slide
for solution*

Exercise 43 - continued

$$T(s) = \frac{5440(\tau s + 1)}{s^3 + 28s^2 + (432 + 5440\tau)s + 5440}$$

Matlab commands:

```
H = tf([5440*t 5400],[1 28 432+5440*t 5440]);
```

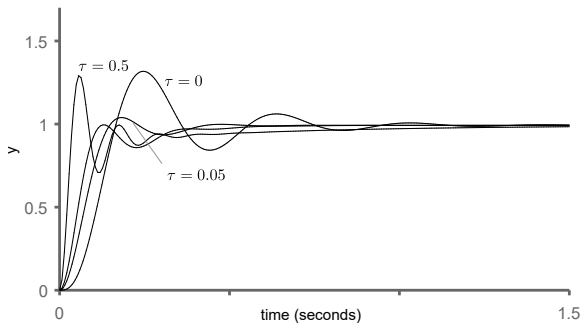
```
infostep(H)
```

```
damp(H)
```

τ	T_r	T_s	P.O.	zero	pole
0	0.16	0.89	37%	N.A.	-20, $-4 \pm 16j$
0.05	0.14	0.39	4.5%	1/0.05	-10.4, $-8.77 \pm 21j$
0.1	0.10	0.49	0%	1/0.1	-6.5, $-10.7 \pm 26j$
0.5	0.04	1.05	29.2%	1/0.5	-1.75, $-13.2 \pm 54j$

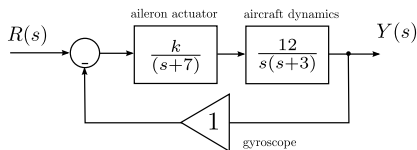
Exercise 43 - continued

```
t = 0;  
H1 = tf([5440*t 5400],[1 28 432+5440*t 5440]);  
step(H1);
```



Exercise 44

The roll control of an aircraft is shown. The goal is to select a suitable K so that the response to a step command $r(t) = A$ will provide a fast response with an overshoot of less than 20%.

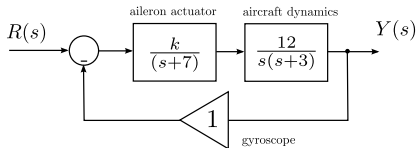


Steps for designing the controller:

- **(a)** Determine the closed-loop transfer function
- **(b)** Determine the poles for $K = 0.7, 3,$ and 6 ;
- **(c)** Using the concept of dominant poles find the expected overshoot
- **(d)** Plot the actual response with Matlab and compare it with (c)

Exercise 44 - continued

(a) The closed-loop transfer function



$$Y(s) = \frac{12K}{s(s+3)(s+7) + 12K} \cdot R(s)$$

$$Y(s) = \frac{12K}{s^2 + 10s^2 + 21s + 12K} R(s)$$

Exercise 44 - continued

(b) Finding the poles

$$T(s) = \frac{12k}{s(s+3)(s+7) + 12k} = \frac{12k}{s^3 + 10s^2 + 21s + 12k} \quad (13)$$

$$s^3 + 10s^2 + 21s + 12k = 0$$

$$k = 0.7 \quad \begin{cases} s_1 = -7.27 \\ s_2 = -2.21 \\ s_3 = -0.52 \end{cases}$$

$$k = 3 \quad \begin{cases} s_1 = -7.91 \\ s_{23} = -1.04 \pm 1.86j \end{cases}$$

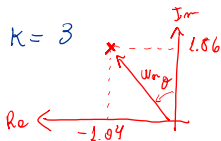
$$k = 4 \quad \begin{cases} s_1 = -8.453 \\ s_{23} = -0.74 \pm 2.81j \end{cases}$$

Exercise 44 - continued

(c) Overshoot considering the dominant poles ($k = 0.7, 3, \text{ and } 6$).

$$T(s) = \frac{12k}{s(s+3)(s+7) + 12k} = \frac{12k}{s^3 + 10s^2 + 21s + 12k} \quad (14)$$

$K = 0.3 \rightarrow$ poles are real P.O. = 0



$$\theta = \tan^{-1}\left(\frac{1.04}{1.86}\right) = 29^\circ$$

$$\zeta = \sin(29^\circ) = 0.488$$

$$\text{P.O.} = 100 e^{\frac{-\pi \zeta}{\sqrt{1-\zeta^2}}} = 17\%$$

$K = 6$

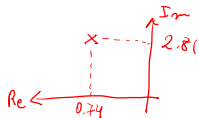
$$\theta = \tan^{-1}\left(\frac{0.74}{2.81}\right)$$

$$\theta = 14^\circ$$

$$\text{P.O.} = 100 e^{\frac{-\pi \zeta}{\sqrt{1-\zeta^2}}} = 43\%$$

$$\omega_n = \sqrt{0.74^2 + 2.81^2} = 2.9058 \text{ rad/s}$$

$$T_s = \frac{4}{\omega_n \zeta} = 3.42 \text{ //}$$



Exercise 44 - continued

(d) Step-unit response using Matlab

Exercise 44 - continued

(c) Overshoot considering the dominant poles ($k = 0.7, 3, \text{ and } 6$).

$$T(s) = \frac{12k}{s(s+3)(s+7) + 12k} = \frac{12k}{s^3 + 10s^2 + 21s + 12k} \quad (15)$$

See previous slides.

Next class...

- Stability