

MECE 3350U  
Control Systems

## Lecture 5

### Effect of Pole Locations

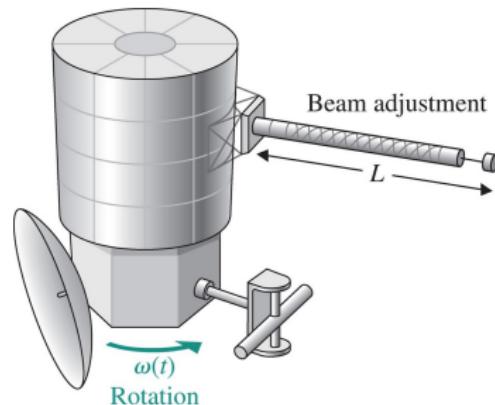
## Outline of Lecture 5

By the end of today's lecture you should be able to

- Understand the concept of transient response
- Observe the influence of the pole locations in the temporal response
- Find the temporal response of a system for a given input

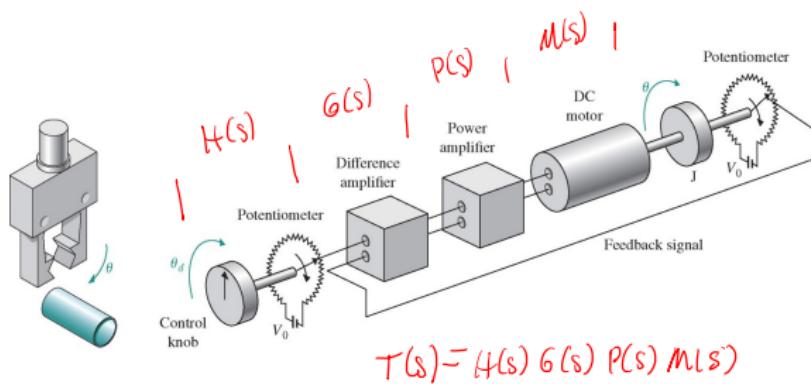
## Applications

The rotational velocity of the satellite is adjusted by changing the length of the beam. How can we determine the shape of the transient response?



# Applications

A robot gripper is to be controlled by a DC motor. How can we determine the transient response of the gripper's position?



## From the last lecture

A transfer function can be written as

$$H(s) = \frac{N(s)}{D(s)} = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0} \quad (1)$$

with  $n \geq m$ . The zeros  $z_i$  are the roots of

$$N(s) = 0$$

Thus:

$$\boxed{\lim_{s \rightarrow z_i} N(s) = 0} \quad (2)$$

The poles  $p_i$  are the roots of

$$D(s) = 0$$

Thus:

$$\boxed{\lim_{s \rightarrow p_i} H(s) = \infty} \quad (3)$$

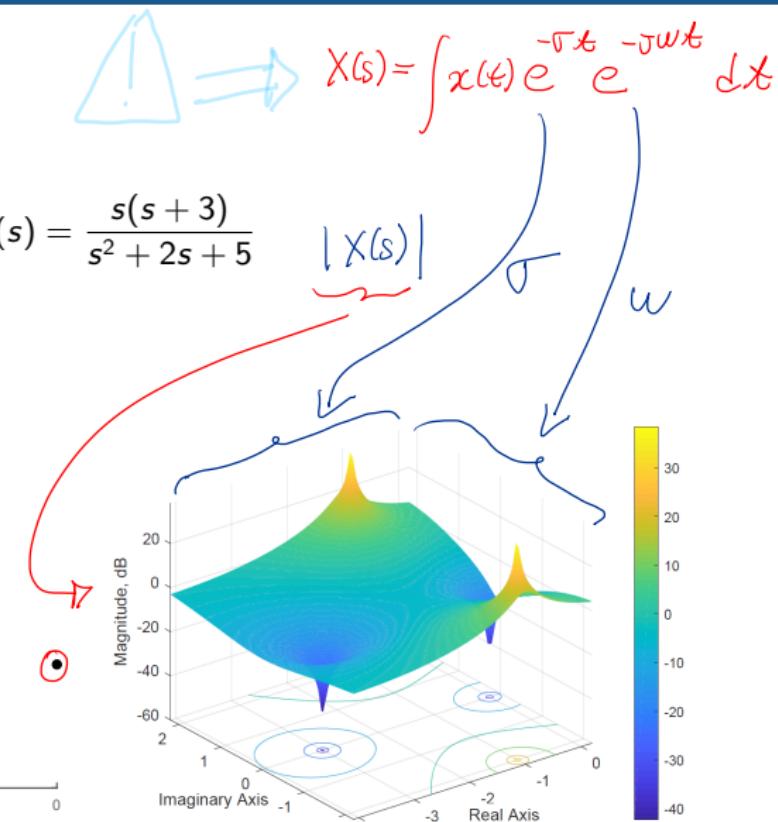
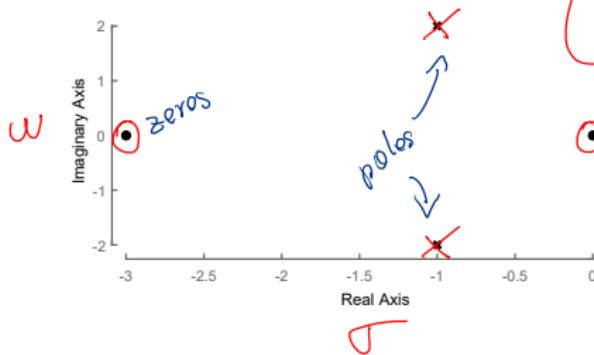
## Poles and zeros

Consider the following function:

$$F(s) = \frac{s(s+3)}{s^2 + 2s + 5}$$

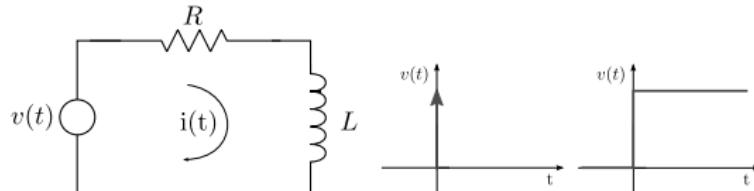
→ Poles:  $-1 + 2j, -1 - 2j$

→ Zeros:  $0, -3$



## First order systems

Consider the RL circuit shown.



$$V(s) = (R + Ls)I(s)$$

$$H(s) = \frac{I(s)}{V(s)} = \frac{1}{Ls + R} = \frac{1/R}{s(L/R) + 1}$$

**Time constant:** Characterizes the response to a step input of a first-order system.

$$\tau = \frac{L}{R} \quad (4)$$

→ The denominator must be in the form of  $\tau s + 1$

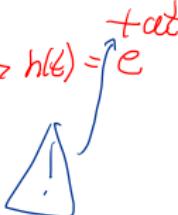
## First order transfer functions

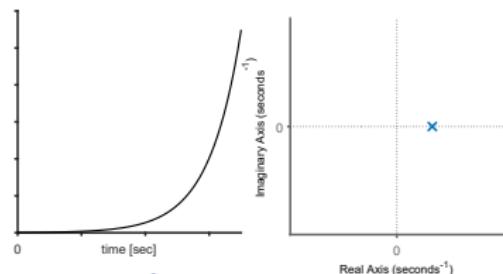
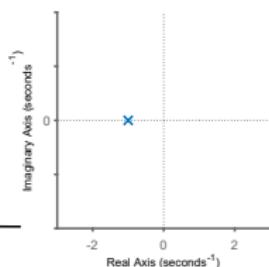
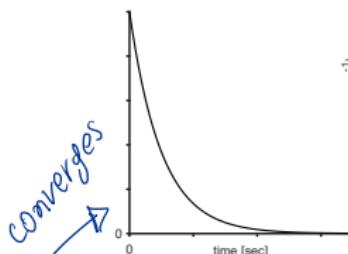
Impulse response:  $v(t) = \delta(t) \Rightarrow V(s) = 1$

$$I(s) = \frac{1}{R} \frac{1}{\tau s + 1} = \frac{1}{\tau R} \left( \frac{1}{s + \frac{1}{\tau}} \right)$$

The pole is  $s = -1/\tau$ . The time response is:

$$i(t) = \frac{1}{\tau R} e^{-\frac{t}{\tau}}$$

$$H(s) = \frac{1}{s+a} \rightarrow h(t) = e^{-at}$$
$$H(s) = \frac{1}{s-a} \rightarrow h(t) = e^{+at}$$




If  $\tau > 0$ , the pole is on the left-half s-plane.

If  $\tau < 0$ , the pole is on the right-half s-plane.

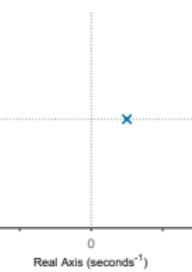
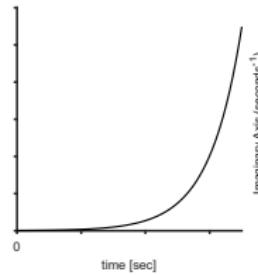
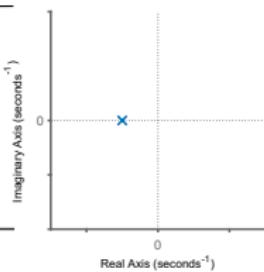
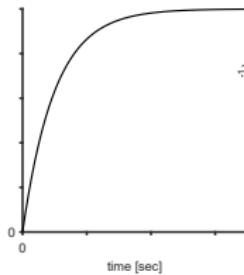
## First order transfer functions

Step response:  $v(t) = u(t) \Rightarrow V(s) = \frac{1}{s}$

$$I(s) = \frac{1}{\tau R} \left( \frac{1}{s} \frac{1}{s + \frac{1}{\tau}} \right) = \frac{1}{\tau R} \left( \frac{1}{s} \right) \left( \frac{1}{s + \frac{1}{\tau}} \right) = \frac{1}{\tau R} \left( \frac{k_1}{s} + \frac{k_2}{s + \frac{1}{\tau}} \right)$$

Solving for the partial fraction coefficients:  $k_1 = \tau$ ,  $k_2 = -\tau$ , thus:

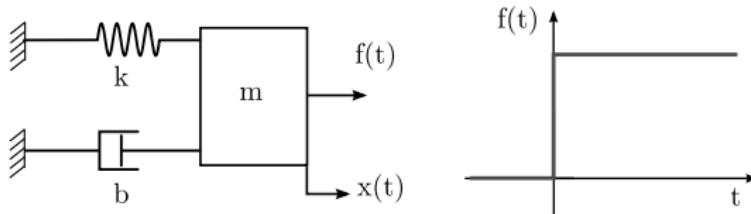
$$i(t) = \frac{1}{R} \left( 1 - e^{-\frac{t}{\tau}} \right)$$



If  $\tau > 0$ , the pole is on the left-half s-plane.

If  $\tau < 0$ , the pole is on the right-half s-plane.

## Second order transfer functions



Transfer function: Standard form

$$H(s) = \frac{X(s)}{F(s)} = \frac{1}{ms^2 + bs + k} = \frac{1}{m} \left( \frac{1}{s^2 + \frac{b}{m}s + \frac{k}{m}} \right)$$

In standard form we have

$$H(s) = \frac{1}{k} \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (5)$$

where:

$\Rightarrow \zeta = \frac{b}{2\sqrt{mk}}$ : Dimensionless **damping ratio**

$\Rightarrow \omega_n = \sqrt{\frac{k}{m}}$ : Natural frequency (rad/s)

## Second order response

Let us now analyse the response to a step input of a second order system

$$X(s) = \frac{1}{k} \left( \frac{1}{s} \right) \left( \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) \quad (6)$$

The poles of the transfer function are:

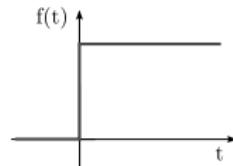
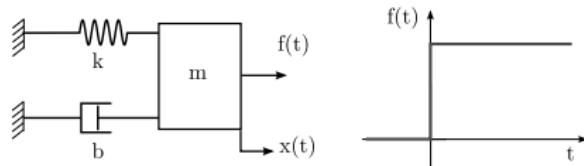
$$s = \frac{-2\zeta\omega_n \pm \sqrt{(2\zeta\omega_n)^2 - 4\omega_n^2}}{2} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1} \quad (7)$$

Thus:

*poles* →  $s_1 = \omega_n \left( -\zeta + \sqrt{\zeta^2 - 1} \right)$       *poles can be real or imaginary. depending on  $\zeta$*   
 $s_2 = \omega_n \left( -\zeta - \sqrt{\zeta^2 - 1} \right)$

Roots can be real or complex ⇒ Inverse transformation ?

## Second order response



$$X(s) = \frac{1}{k} \left( \frac{1}{s} \right) \left( \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) \quad (8)$$

**Case 1:**  $\zeta \geq 1$ , (lots of damping)

$$s_1 = \omega_n \left( -\zeta + \sqrt{\zeta - 1} \right) \quad \text{if } \zeta > 1, s_1, s_2 \in \mathbb{R}$$
$$s_2 = \omega_n \left( -\zeta - \sqrt{\zeta - 1} \right) \quad \text{thus } X(s) = \frac{1}{ks} \frac{1}{(s+a)(s+b)}$$

Roots are negative real numbers. Partial fraction expansion yields:

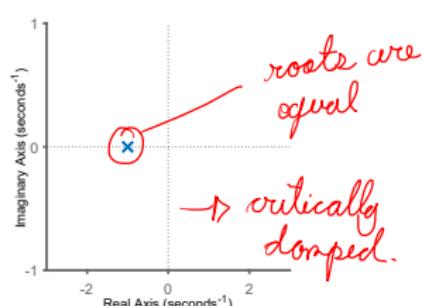
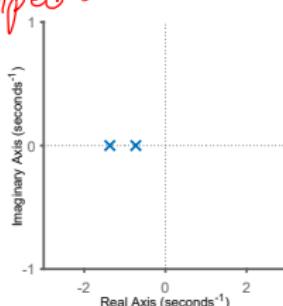
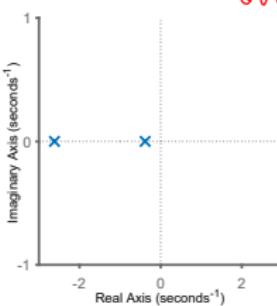
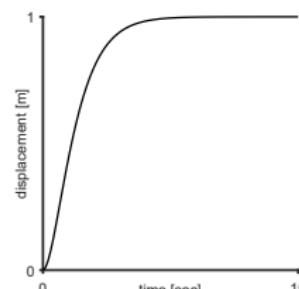
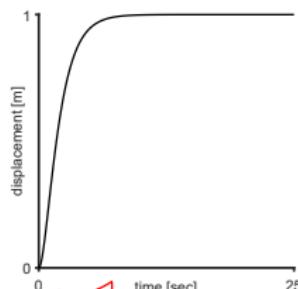
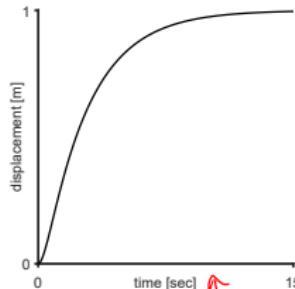
$$a, b, \in \mathbb{R}$$

$$X(s) = \frac{1}{m} \left( \frac{k_1}{s} + \frac{k_2}{(s + a_1)} + \frac{k_3}{(s + a_2)} \right) \quad (9)$$

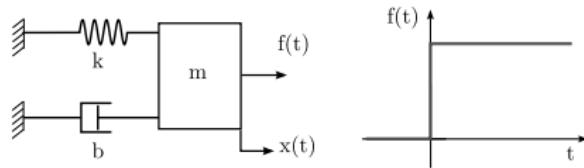
## Overdamped system

Example:  $m = 1 \text{ kg}$ ,  $k = 1 \text{ N/m}$

$b = 3 \text{ Ns/m}$ ,  $\zeta = 1.5$ ;       $b = 2.1 \text{ Ns/m}$ ,  $\zeta = 1.05$ ;       $b = 2 \text{ Ns/m}$ ,  $\zeta = 1$ .



## Second order response



$$X(s) = \frac{1}{k} \left( \frac{1}{s} \right) \left( \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) \quad (10)$$

**Case 2:**  $0 < \zeta < 1$ , (some damping)

$$s_1 = \omega_n \left( -\zeta + \sqrt{\zeta - 1} \right)$$

$$s_2 = \omega_n \left( -\zeta - \sqrt{\zeta - 1} \right)$$

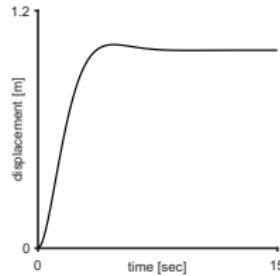
Roots are complex conjugate numbers with a negative real part. Thus:

$$x(t) = \frac{1}{k} \left[ 1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin \left( \omega_n \sqrt{1-\zeta^2} t + \cos^{-1} \zeta \right) \right] \quad (11)$$

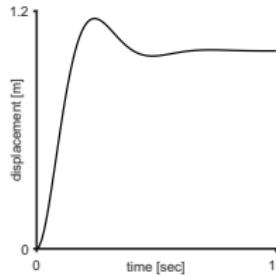


# Underdamped system

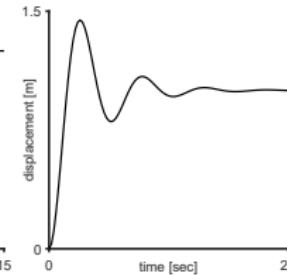
$$b = 1.5, \zeta = 0.75$$



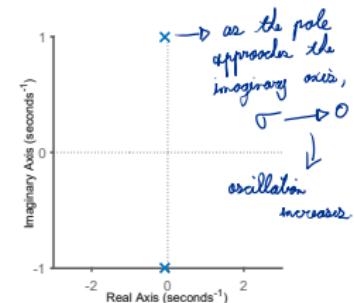
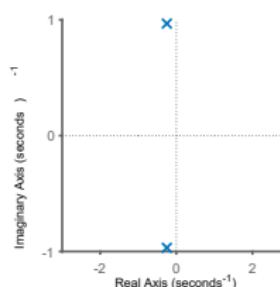
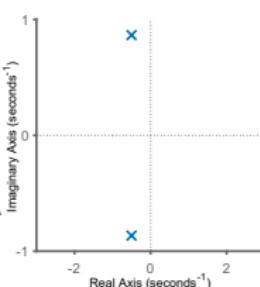
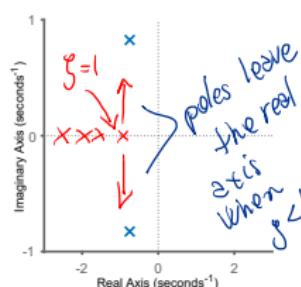
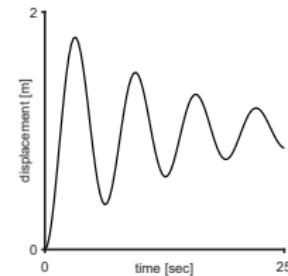
$$b = 1, \zeta = 0.5;$$



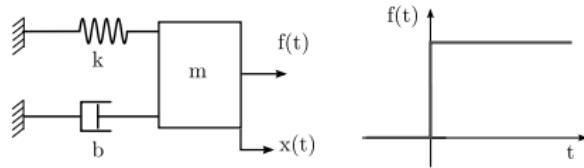
$$b = 0.5, \zeta = 0.25,$$



$$b = 0.1, \zeta = 0.05$$



## Second order response



$$X(s) = \frac{1}{k} \left( \frac{1}{s} \right) \left( \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) \quad (12)$$

**Case 3:**  $\zeta = 0$ , (no damping)

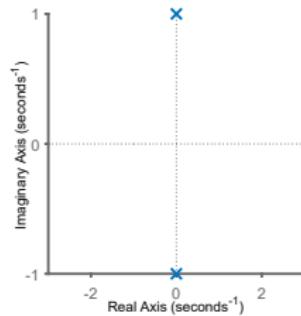
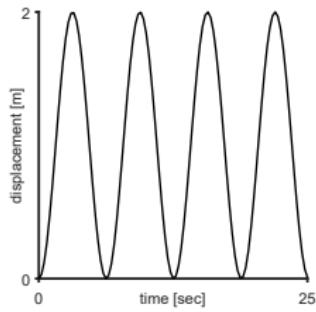
$$= 0$$

$$s_1 = \omega_n \left( -\zeta + \sqrt{\zeta - 1} \right)$$
$$s_2 = \omega_n \left( -\zeta - \sqrt{\zeta - 1} \right)$$

Roots are purely complex conjugate numbers. Thus:

$$X(s) = \frac{1}{k} \left( \frac{1}{s} \right) \left( \frac{\omega_n^2}{s^2 + \omega_n^2} \right) \rightarrow x(t) = \frac{1}{k} [1 - \cos(\omega_n t)] \quad (13)$$

## Undamped system



if  $\sigma = 0$ , poles  
are purely  
imaginary and lie  
on the imaginary  
axis ( $\sigma = 0$ )  
(no exponential)

The frequency of oscillation for an undamped system is called the natural frequency.

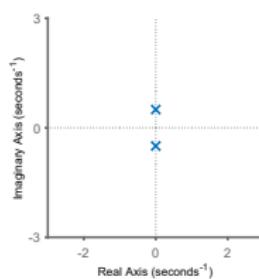
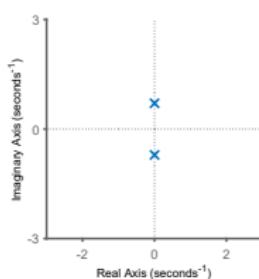
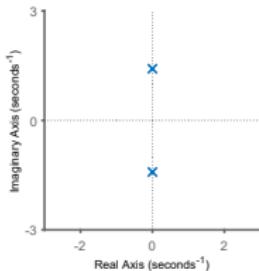
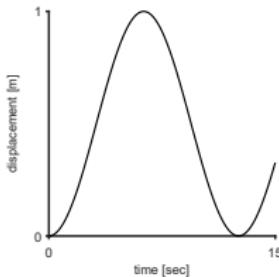
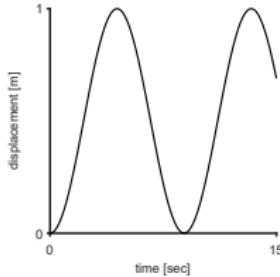
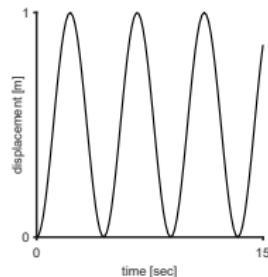
In our example:

$$\omega_n = \sqrt{\frac{k}{m}} \quad (14)$$

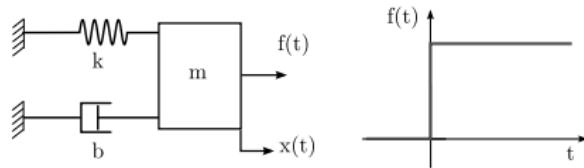
# Natural frequency

The frequency the system oscillates when  $\zeta = 0$ . Example:  $b = \zeta = 0$ ,  $k = 1$ .

$$m = 1, \omega_n = 1 \text{ rad/s}; \quad m = 2, \omega_n = 0.71 \text{ rad/s}; \quad m = 4, \omega_n = 0.5 \text{ rad/s};$$



## Second order response



$$X(s) = \frac{1}{k} \left( \frac{1}{s} \right) \left( \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) \quad (15)$$

**Case 4:**  $\zeta < 0$ , (hypothetical negative damping)

$$s_1 = \omega_n \left( -\zeta + \sqrt{\zeta - 1} \right), \quad s_2 = \omega_n \left( -\zeta - \sqrt{\zeta - 1} \right)$$

Roots (real or imaginary) have positive real parts. Possible solutions are:

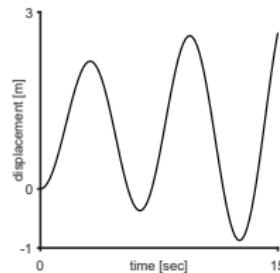
$$x(t) = k(1 + k_2 e^{s_1 t} + k_3 e^{s_2 t}) \quad (16)$$

$$x(t) = \frac{1}{k} \left[ 1 - \frac{1}{\sqrt{1-\zeta^2}} e^{| \zeta | \omega_n t} \sin \left( \omega_n \sqrt{1-\zeta^2} t + \cos^{-1} \zeta \right) \right] \quad (17)$$

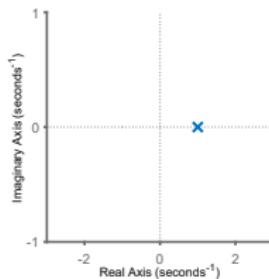
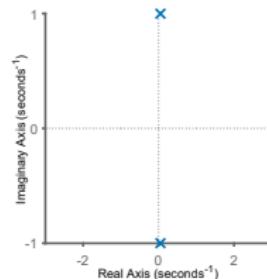
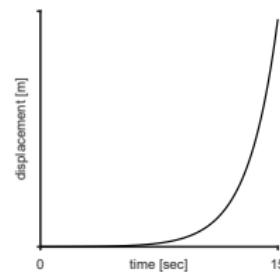
↑ increases over time

## Unstable system

$$b = -0.1 \text{ Ns/m};$$

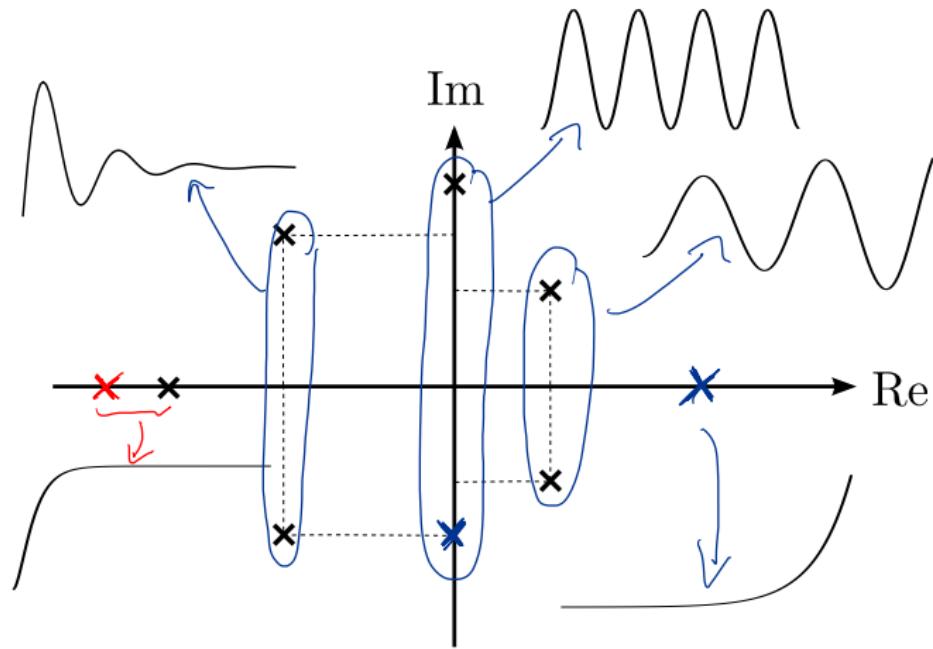


$$b < -1 \text{ Ns/m};$$

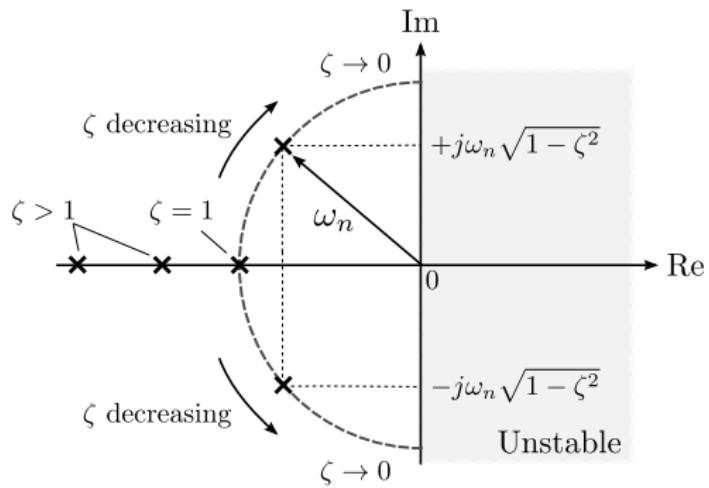


unstable : real part of the poles is positive (at least one)

## Summary



Damping ratio	Roots	Systems response
$\zeta > 1$	Distinct real	overdamped
$\zeta = 1$	Equal real	damped
$0 < \zeta < 1$	Complex conjugate	underdamped
$\zeta = 0$	Purely imaginary	undamped
$\zeta < 0$	Positive	unstable



## Location of poles in the s-plane

For a second order system, the poles are

$$s = \zeta\omega_n \pm j\omega_n\sqrt{1 - \zeta^2}$$

$$s = -\sigma \pm j\omega_d$$

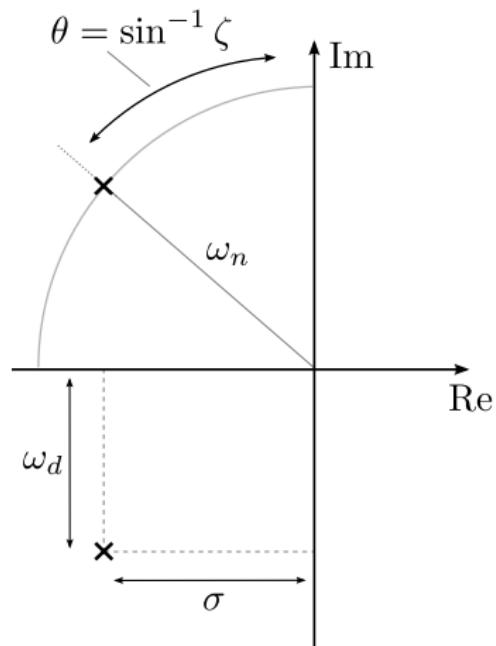
where  $\sigma = \zeta\omega_n$ , and  $\omega_d = \omega_n\sqrt{1 - \zeta^2}$

→ The magnitude of  $s$  is

$$|s| = \sqrt{(\zeta\omega_n)^2 + (\omega_n\sqrt{1 - \zeta^2})^2} = \omega_n$$

→ The angle to the imaginary axis is

$$\sin \theta = \frac{\zeta\omega_n}{\omega_n} \rightarrow \theta = \sin^{-1} \zeta$$



## Exercise 21

Discuss the correlation between the poles of

$$H(s) = \frac{2s + 1}{s^2 + 2s + 5} \quad (18)$$

and the impulse response of the system and find the exact impulse response.

### Procedure:

- Calculate the damping ratio and the natural frequency
- Calculate inverse transform

Homework

## Exercise 21 - continued

polar are

$$s^2 + 2s + 5 = 0$$

$$s = -1 + 2i$$

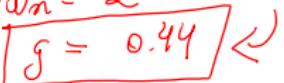
$$s' = -1 - 2i$$

$$H(s) = \frac{2s+1}{s^2 + 2s + 5}$$

$$\omega_n = \sqrt{5}$$

$$2g\omega_n = 2$$

$$g = 0.44$$



$$H(s) = \frac{2s+1}{(s+1-2i)(s+1+2i)} = \frac{A}{s+1+2i} + \frac{\beta}{s+1-2i}$$

$$A(s+1-2i) + B(s+1+2i) = 2s+1$$

$$\begin{cases} A+B=2 \\ A-2Ai+B+2Bi=1 \end{cases}$$

> solving  $\rightarrow A = 1 - \frac{1}{4}i$

$$\beta = 1 + \frac{1}{4}i$$

## Exercise 21 - continued

$$H(s) = \frac{1 - \frac{1}{4}i}{s + 1 + 2i} + \frac{1 + \frac{1}{4}i}{s + 1 - 2i} \quad \Bigg) \mathcal{L}^{-1}$$

$$h(t) = \left(1 - \frac{1}{4}i\right) e^{(-1-2i)t} + \left(1 + \frac{1}{4}i\right) e^{(-1+2i)t}$$

$$h(t) = \left(1 - \frac{1}{4}i\right) e^{-t} e^{-2it} + \left(1 + \frac{1}{4}i\right) e^{-t} e^{2it}$$

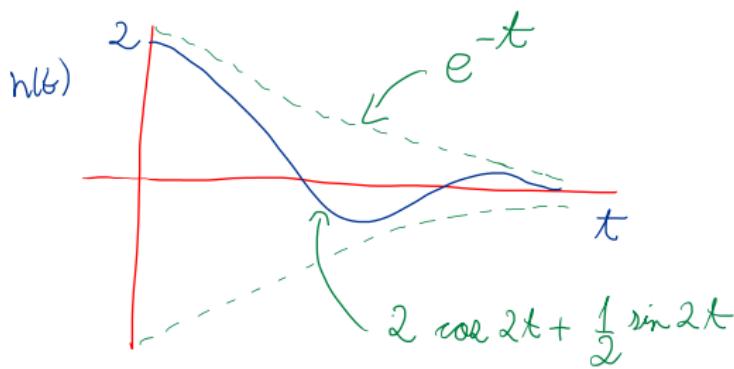
$$h(t) = e^{-t} \left[ e^{-2it} + e^{2it} + \frac{1}{4}i(e^{-2it} + e^{2it}) \right]$$

## Exercise 21 - continued

$$\cos \alpha = \frac{1}{2} (e^{i\alpha} + e^{-i\alpha}) \quad , \quad \sin \alpha = \frac{1}{2i} (e^{i\alpha} - e^{-i\alpha})$$

thus,

$$h(t) = e^{-t} \left( 2 \cos(2t) + \frac{1}{2} \sin(2t) \right) //$$



## Exercise 22

Consider the system of the form

$$H(s) = \frac{9}{s^2 + bs + 9} \quad (19)$$

Calculate and sketch the response to a unit step input for the following cases

$$\rightarrow b = 9$$

$$\rightarrow b = 0$$

$$\rightarrow b = 2$$

$$\rightarrow b = 6$$

$$\rightarrow v(t) = 1$$

$$V(s) = \frac{1}{s}$$

## Exercise 22 - continued

$$w_n = \sqrt{g} = 3 \text{ rad/s}$$

$$\zeta = \frac{g}{2w_n} = 1.5$$

$\rightarrow$  real distinct roots  $\rightarrow$  overdamped.

$$H(s) = \frac{9}{\underbrace{s^2 + 9s + 9}_{s^2 + 2\zeta w_n s + w_n^2}} \frac{1}{s} \quad (20)$$

roots are

$$s^2 + 9s + 9 = 0$$

$$\begin{cases} s = -7.854 \\ s = -1.146 \end{cases}$$

$$H(s) = \frac{A}{s + 7.854} + \frac{B}{s + 1.146} + \frac{C}{s}$$

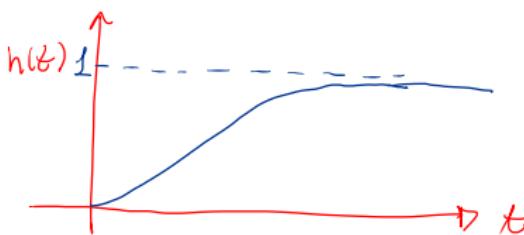
solving partial fraction

$$A = 0.171$$

$$B = -1.171$$

$$C = 1$$

$$h(t) = 0.171 e^{-7.854 t} - 1.171 e^{-1.146 t} + 1$$



## Exercise 22 - continued

$$b=0$$

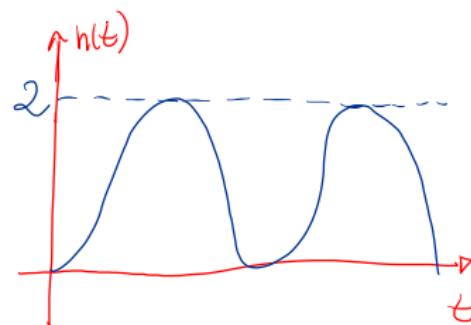
$$H(s) = \frac{9}{s^2 + 9} \frac{1}{s} \quad (21)$$

$$H(s) = \frac{As+B}{s^2+9} + \frac{C}{s}$$

$$\begin{aligned} A &= -1 \\ B &= 0 \\ C &= 1 \end{aligned}$$

$$H(s) = \frac{1}{s} - \frac{s}{s^2+9} \quad \Downarrow \mathcal{L}^{-1}$$

$$h(t) = 1 - \cos(3t)$$



## Exercise 22 - continued

$$b=2$$

$$\omega_n = 3 \text{ rad/s}$$

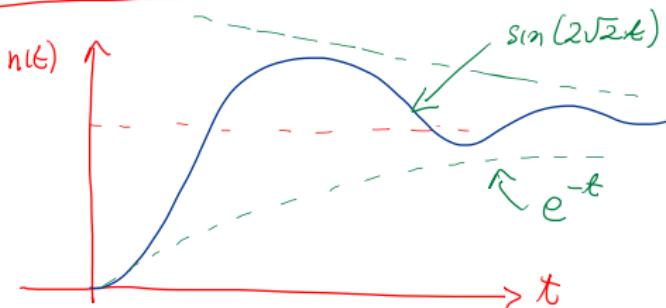
$$2\zeta\omega_n = 2$$

$\zeta = \frac{1}{3} < 1 \rightarrow \text{poles are complex conjugate}$

$$H(s) = \frac{9}{s^2 + 2s + 9} \frac{1}{s} \quad (22)$$

$$h(t) \approx \frac{9}{2\sqrt{2}} e^{-t} \sin(2\sqrt{2}t)$$

see Exercise 21.  
Development is the same.



## Exercise 22 - continued

$$\omega_n = 3$$
$$2\zeta\omega_n = 6$$

critically damped

$$\boxed{\zeta = 1}$$

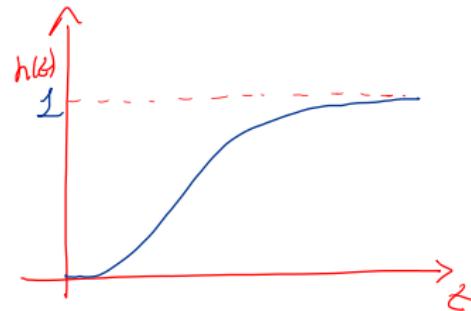
$$H(s) = \frac{9}{s^2 + 6s + 9} \frac{1}{s} \quad (23)$$

roots are  $-3, -3$ .

$$H(s) = \frac{9}{(s+3)^2} \cdot \frac{1}{s} = \frac{A}{s} + \frac{B}{(s+3)^2} + \frac{C}{s+3}$$

$$\begin{aligned} A &= 1 \\ B &= -3 \\ C &= -2 \end{aligned}$$

$$h(t) = 1 - 3te^{-3t} - e^{-3t}$$



Next class...

- Block diagrams