

MECE 3350U  
Control Systems

Lecture 13  
PID Controllers

## Outline of Lecture 13

By the end of today's lecture you should be able to

- Define a PID controller
- Understand the influence of the controller in the temporal response
- Understand the practical applications of PID control

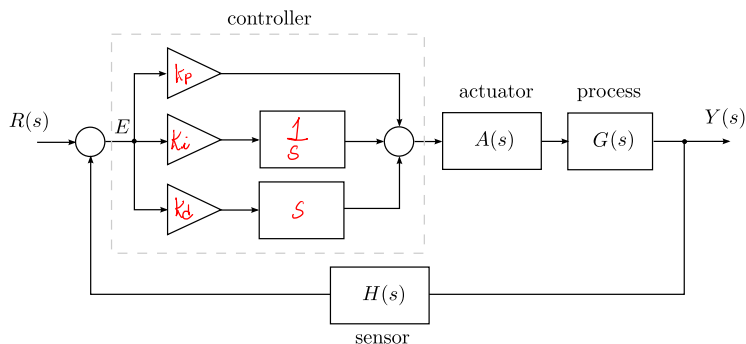
## Applications

Proportional-Integral-Derivative (PID) controllers are used in most automatic process control applications in industry.



More than 90% of industrial controllers are PID.

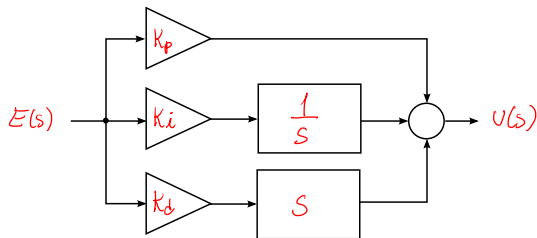
## PID controller



The command signal is a function of

- The magnitude of the current error: proportional gain
- The integral of the error over time: integral gain
- The time rate change of the error: derivative gain

## PID controller



$$u(t) = k_p e(t) + k_i \int_0^t e(t) dt + k_d s e(t)$$

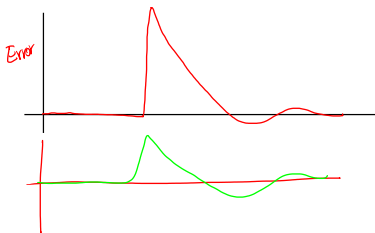
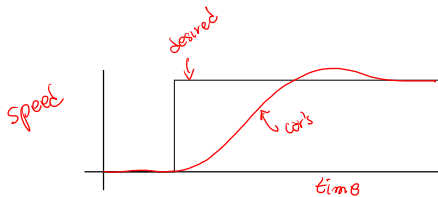
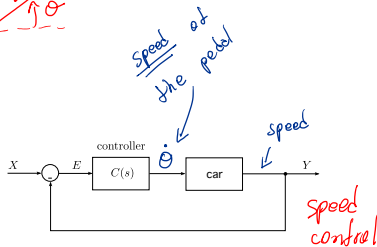
$$U(s) = k_p E(s) + k_i \frac{1}{s} E(s) + k_d s E(s)$$

$$U(s) = \left( k_p + k_i \frac{1}{s} + k_d s \right) E(s)$$

# Proportional controller

$$G(s) = k_p, \text{ with } k > 0.$$

$$\dot{\theta}(t) = k_p e(t)$$



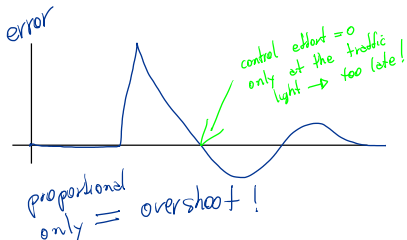
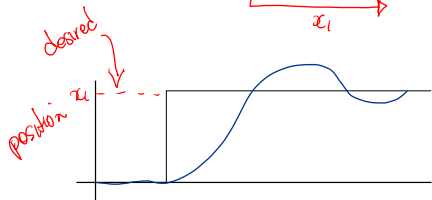
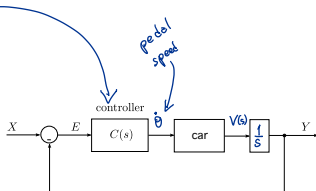
proportional controller  $\rightarrow$  controller output

# Proportional-derivative (PD) controller

$$G(s) = k_p + k_d s, \text{ with } k > 0.$$

$$\dot{\theta}(t) = k_p e(t) + k_d \frac{d}{dt} e(t)$$

*= 0*

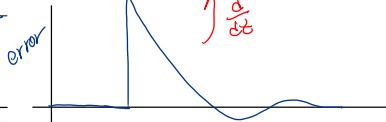
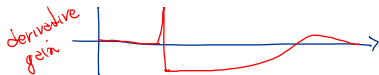
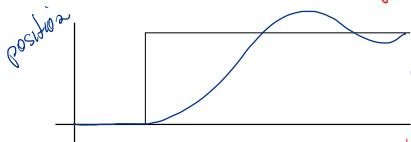
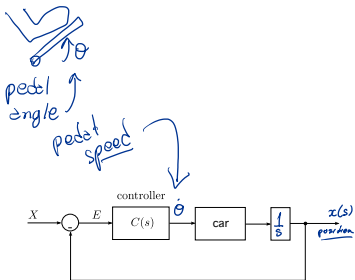


# Proportional-derivative (PD) controller

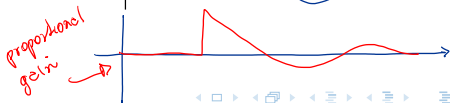
$$G(s) = k_p + k_d s, \text{ with } k > 0.$$

$$\dot{\theta}(t) = k_p e(t) + k_d \frac{d}{dt} e(t)$$

$\neq 0$



$P + D = \text{less overshoot}$



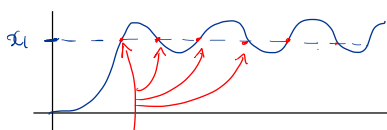
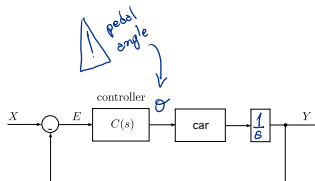
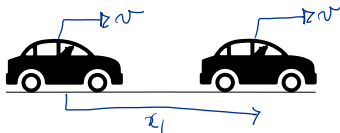


# Proportional-integral-derivative (PID) controller

$$G(s) = k_p + k_d s + k_d \frac{1}{s}, \text{ with } k > 0.$$

$$\theta(t) = k_p e(t) + k_d \frac{d}{dt} e(t) + k_i \int e(t) dt$$

objective  
 $x_1 = 0$

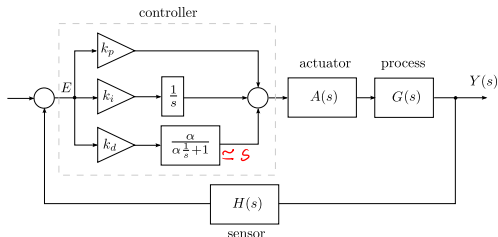


$\theta = 0$  ! = steady-state error



eliminates steady state error

## PID implementation



$$u(t) = k_p e(t) + k_i \int_0^t e(t) dt + k_d \frac{d}{dt} e(t)$$

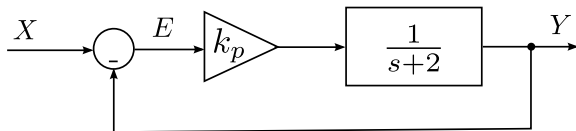
→ Proportional gain: Consider only the current error

→ Integral gain: Looks at the past error

→ Derivative gain: "Anticipates" the future error

## PID controller

Effect of  $k_p$



The transfer function is

$$T(s) = \frac{k_p}{s + k_p + 2} \quad (1)$$

The time constant is  $1/(k_p + 2)$ .

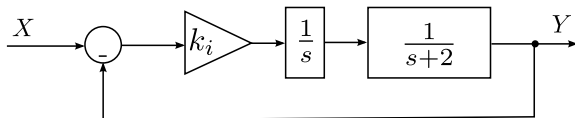
The steady-state error for  $x(t) = 1$  is

$$e(\infty) = u(t) - \lim_{s \rightarrow 0} [sF(s)] = 1 - \lim_{s \rightarrow 0} s \frac{k_p}{s + k_p + 2} \frac{1}{s} = 1 - \frac{k_p}{k_p + 2} \quad (2)$$

*k<sub>p</sub> reduces e(∞)*

## PID controller

Effect of the integrator and  $k_i$  on the transient response



The transfer function is

$$T(s) = \frac{k_i}{s(s+2) + k_i} = \frac{k_i}{s^2 + 2s + k_i} \quad (3)$$

where  $\omega_n = \sqrt{k_i}$  and  $\zeta = 1/\sqrt{k_i}$ .

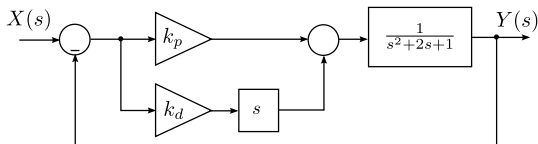
The **damping ratio decreases** with  $k_i$ .

Overshoot:  $P.O. = 100e^{-\zeta\pi/\sqrt{1-\zeta^2}} = 100e^{-\pi/\sqrt{k_i-1}}$

⇒ The **overshoot increases** with  $k_i$

## PID controller

Effect of the derivative gain  $k_d$



The transfer function is

$$T(s) = \frac{sk_d + k_p}{s^2 + (2 + k_d)s + 1 + k_p} \quad (4)$$

note the final value does not depend on  $k_d$ , thus it has **no effect** on the steady-state error.

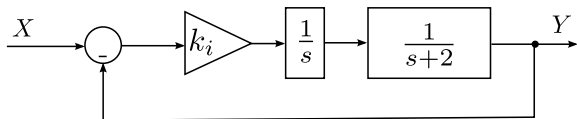
From the characteristic equation:  $\zeta = (2 + k_d)/2(\sqrt{1 + k_p})$ ,  $\omega_n = \sqrt{1 + k_p}$

The overshoot:  $P.O. = 100e^{-\zeta\pi/\sqrt{1-\zeta^2}}$  **decreases** with  $k_d$ .

The settling time:  $T_s = 4\omega_n\zeta$  **decreases** with  $k_d$ .

## PID controller

Effect of the integrator on the steady-state error



The transfer function is

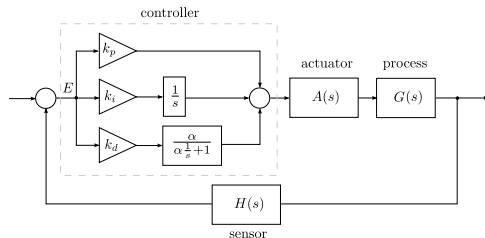
$$T(s) = \frac{k_i}{s(s+2) + k_i} = \frac{k_i}{s^2 + 2s + k_i} \quad (5)$$

Steady-state error

$$e(\infty) = u(t) - \lim_{s \rightarrow 0} [sF(s)] = 1 - \lim_{s \rightarrow 0} s \frac{k_i}{s(s+2) + k_i} \frac{1}{s} = 0 \quad (6)$$

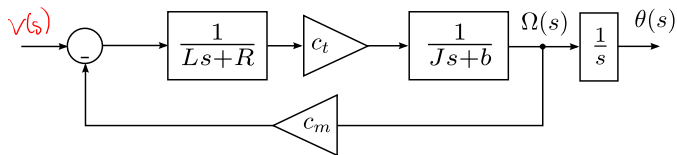
*always  $e(\infty) = 0$  if  $k_i \neq 0$*

## PID gains



PID gain	Overshoot	Settling time	Steady-state error
Increasing $k_p$	Increases	Minimal impact	Decreases
Increasing $k_i$	Increases	Increases	Zero error
Increasing $k_d$	Decreases	Decreases	No impact

## Speed control of a DC motor



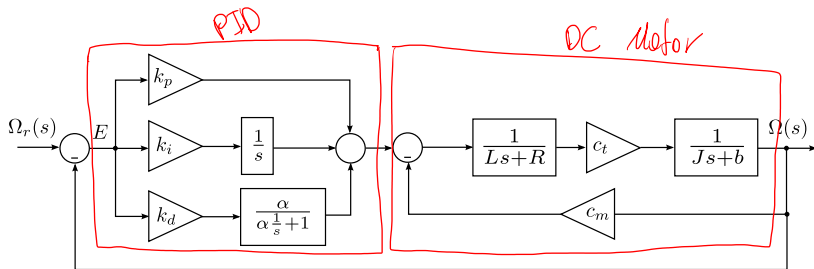
DC motor characteristics:

$$J = 1.13 \times 10^{-2} \text{ Nm} - \text{sec}^2/\text{rad}, \quad b = 0.028 \text{ Nm} - \text{sec}/\text{rad}, \quad L = 0.1 \text{ H}$$

$$R = 0.45 \text{ Ohms}, \quad c_t = 0.067 \text{ Nm/A}, \quad c_m = 0.067 \text{ V-sec/rad}$$



## Speed control of a DC motor



$$\alpha = 100$$

See Simulink  
model posted on B.B.

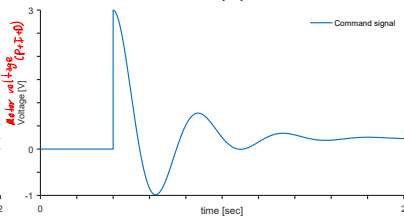
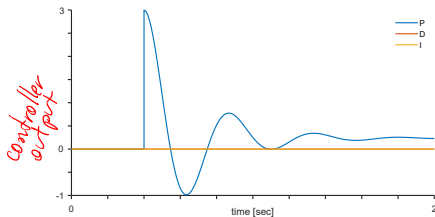
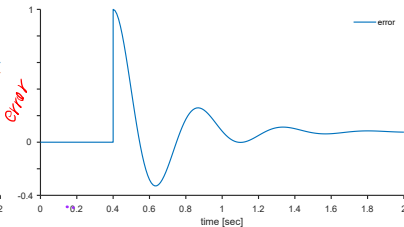
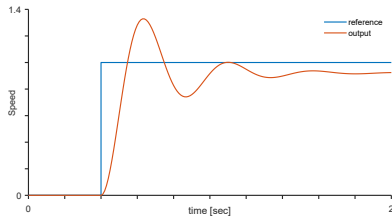
Proportional control:  $k_p = 3$ ,  $k_d = 0$ ,  $k_i = 0$

Proportional-integral control:  $k_p = 3$ ,  $k_d = 15$ ,  $k_i = 0$

PID control:  $k_p = 3$ ,  $k_i = 15$ ,  $k_d = 0.3$

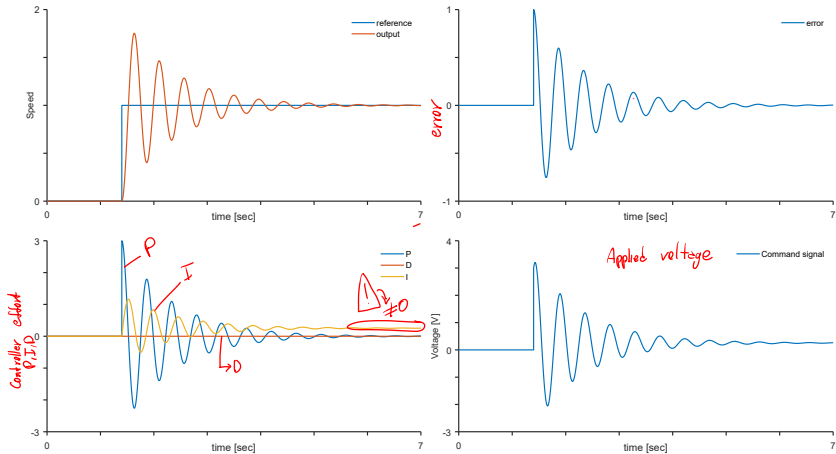
# Speed control of a DC motor

Proportional control:  $k_p = 3$ ,  $k_d = 0$ ,  $k_i = 0$



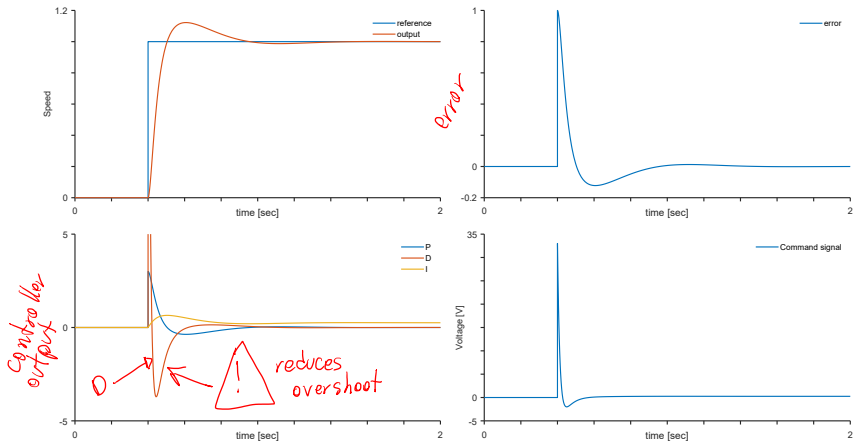
# Speed control of a DC motor

Proportional-integral control:  $k_p = 3$ ,  $k_i = 15$ ,  $k_d = 0$

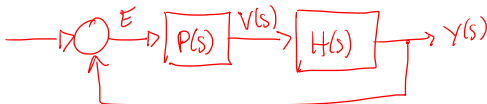


# Speed control of a DC motor

Proportional-integral-derivative control:  $k_p = 3$ ,  $k_d = 15$ ,  $k_i = 0.3$



## Exercise 66



A block diagram of a diesel engine driving load has an transfer function connecting the fuel valve setting  $V(s)$  and the load shaft speed  $Y(s)$  given by

$$H(s) = \frac{Y(s)}{V(s)} = \frac{1}{0.01s^2 + 0.11s + 0.1} \quad (7)$$

Speed control is provided by a PID controlled whose transfer function is

$$P(s) = \frac{V(s)}{E(s)} = 5 + 0.3s + \frac{5}{sT} \quad (8)$$

By using the root-locus method, determine the minimum value  $\tau$  if the complex closed loop dominant poles are to have a damping ratio not less than 0.7.

① write the root-locus function as  $1 + z Z(s) = 0$   $Z(s)$  is a function of  $s$

# Exercise 66 - continued

Zeros  $\rightarrow \begin{cases} s=0 \\ s=-20.5 \pm 9.5i \end{cases}$

$$1 + \tau \left( \frac{0.01s^3 + 0.41s^2 + 5.1s}{5} \right) = 0 \quad (9)$$

$n-m=3$

$g=1 \quad \theta=60^\circ$

$g=2 \quad \theta=180^\circ$

$g=3 \quad \theta=-60^\circ$

$\alpha = \frac{\sum p - \sum z}{3}$

$\alpha = \frac{-20.5 - 20.5 - 0}{3}$

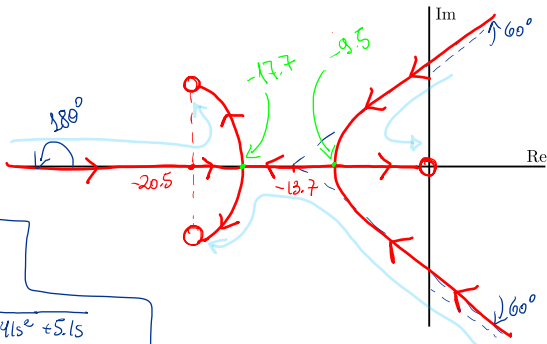
$\alpha = -13.7$

Break away/in points

$Z = p(s)$

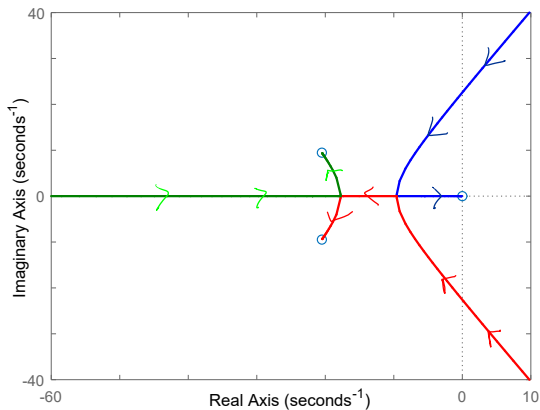
$p(s) = -\frac{5}{0.01s^3 + 0.41s^2 + 5.1s}$

$\frac{dp(s)}{ds} = 0 \rightarrow \begin{cases} s = -9.5 \\ s = -17.7 \end{cases}$

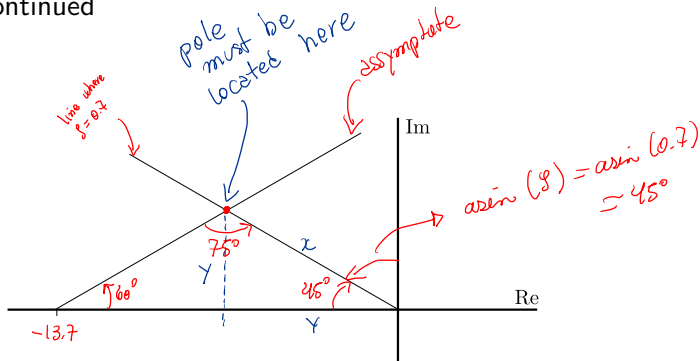


## Exercise 66 - continued

$$1 + \tau \left( \frac{0.01s^3 + 0.41s^2 + 5.1s}{5} \right) = 0 \quad (10)$$



## Exercise 66 - continued



$$\frac{\sin(75^\circ)}{13.7} = \frac{\sin(60^\circ)}{x}$$

$$x = 12.2$$

$$y = x \sin(45^\circ)$$

$$y = 8.7$$

pole is

$$s = -8.7 \pm 8.7j$$



## Exercise 66 - continued

$$s = -8.7 \pm 8.7j \quad \swarrow \text{replace } s \text{ here, find } \tau$$

$$(0.01s^3 + 0.11s^2 + 0.1s)\tau + (0.3s^2 + 5s)\tau + 5 = 0$$

$$\tau = 0.16$$

Centre of the asymptote is constant.  $\forall \tau$

Thus we can estimate the location of the 3 pole as

$$-13.7 = \frac{\sum p - \sum z}{3}$$

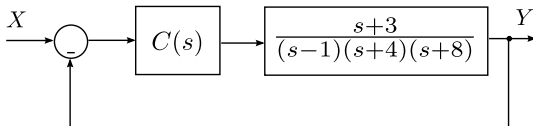
$$-13.7 = \frac{-8.7 - 8.7 - p_2}{3}$$

$$p_2 = -23.6$$

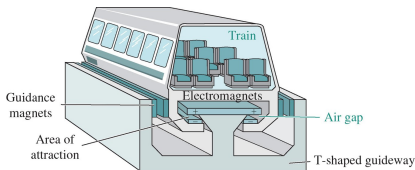
(insignificant pole)

## Exercise 67

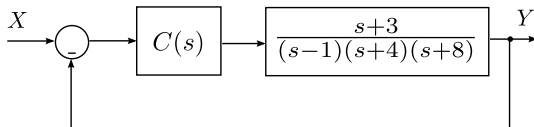
The air gap control system in a magnetically levitated high-speed train is controlled by a PI controller  $G(s)$  have the same  $k_i$  and  $k_p$  gains.  $k_d = 0$



Select the controller gain  $k = k_i = k_p$  so that all of the complex poles have a damping ratio higher than 0.6.



## Exercise 67 - continued



$$K_d = K_i = K$$

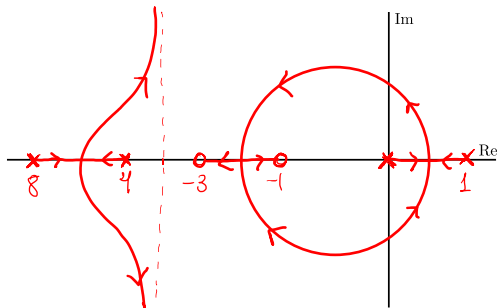
$$C(s) = \frac{K}{s} + K = K \left( \frac{1+s}{s} \right)$$

$$1 + K \frac{(s+1)(s+3)}{s(s+4)(s+8)(s-1)} = 0$$

## Exercise 67 - continued

$$1 + k \frac{(s+1)(s+3)}{s(s-1)(s+4)(s+8)} = 0 \quad (11)$$

$$n-m=2$$

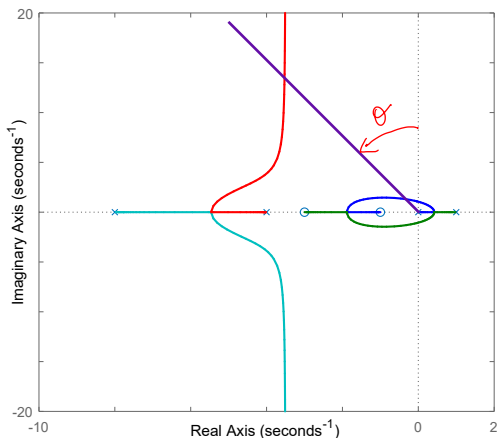


Asymptotes:  $2, 90^\circ, -90^\circ$

Centroid:  $\alpha = \frac{(0 - 4 - 8 + 1) - (-1 - 3)}{2} = -3.5$

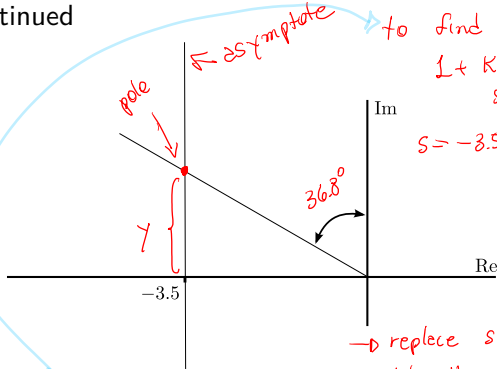
## Exercise 67 - continued

$$1 + k \frac{(s+1)(s+3)}{s(s-1)(s+4)(s+8)} = 0 \quad (12)$$



$\theta = \sin^{-1}(0.6)$   
 desired  
 damping  
 $\theta = 36.8^\circ$

# Exercise 67 - continued



to find K:

$$1 + K \frac{(s+1)(s+3)}{s(s+1)(s+4)(s+8)} = 0$$

$$s = -3.5 + 4.66j \quad \uparrow \text{replace.}$$

→ replace  $s = -3.5 + 4.66j$   
 calculate the magnitude at  $\uparrow = 1$

$$\tan(36.8^\circ) = \frac{3.5}{\gamma}$$

$$\gamma = 4.66$$

$$1 = K \frac{\sqrt{(-3.5+1)^2 + 4.66^2} \sqrt{(-3.5+3)^2 + 4.66^2}}{\sqrt{3.5^2 + 4.66^2} \sqrt{(-3.5+4)^2 + 4.66^2} \sqrt{(-3.5+1)^2 + 4.66^2} \sqrt{5.5^2 + 4.66^2}} = 1$$

pole is  $s = -3.5 \pm 4.66j$

$$K = 46.1$$

Next class...

- Tuning a PID controller